

# Chapter 21

## Analysis of Accelerated Degradation Data

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Based on the authors' text *Statistical Methods for Reliability Data*, John Wiley & Sons Inc. 1998.

July 18, 2002

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# Chapter 21

## Analysis of Accelerated Degradation Data

### Objectives

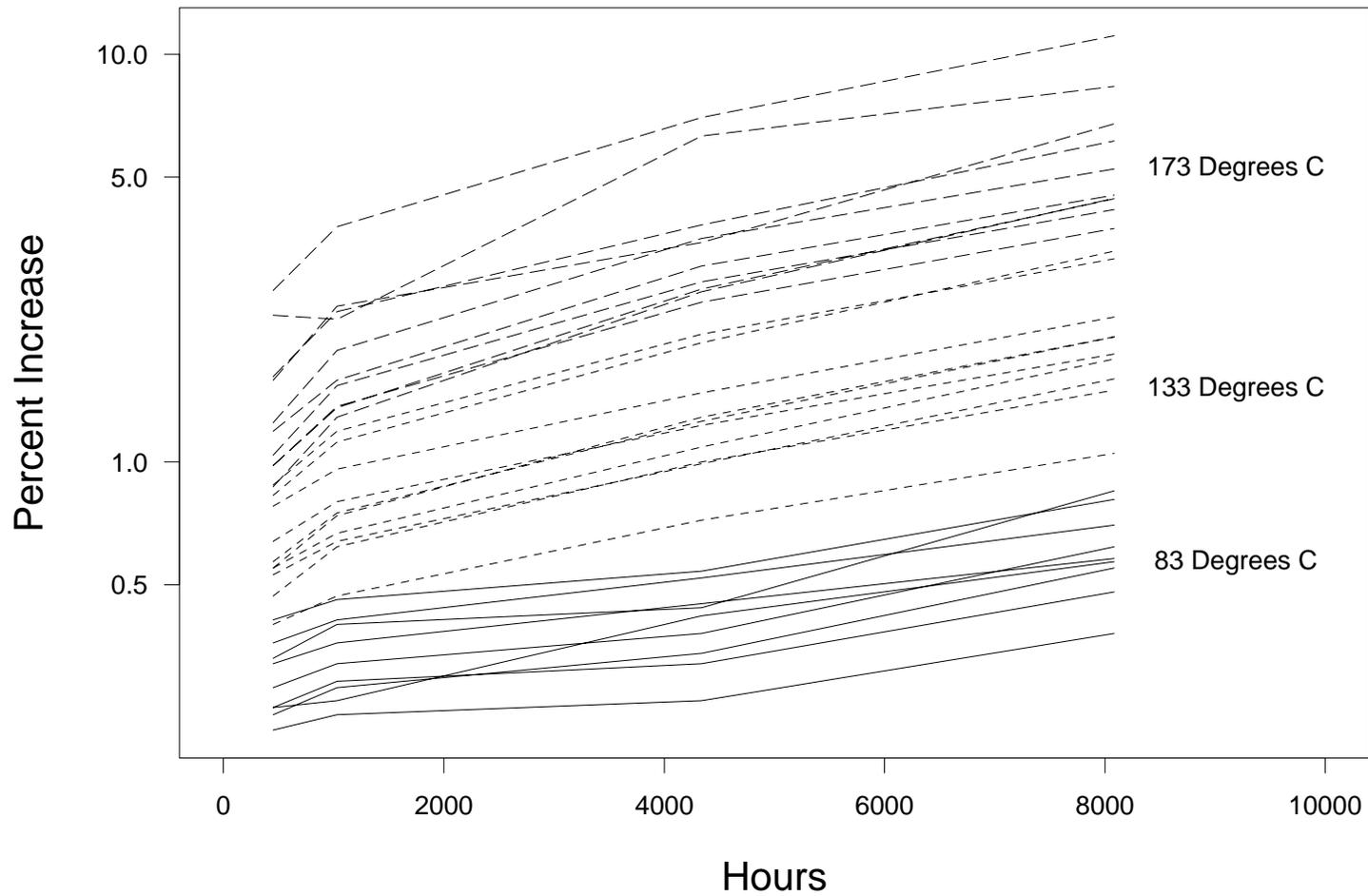
- Show how accelerated degradation tests can be used to assess and improve product reliability.
- Present models, methods of analysis, and methods of inference for accelerated degradation tests.
- Show how to analyze data from accelerated degradation tests.
- Compare accelerated degradation test methods with traditional accelerated life test methods using failure-time data.

## Background

Today's manufacturers face strong pressure to:

- Develop newer, higher technology products in record time.
- Improve productivity, product field reliability, and overall quality.
- Increased the need for **up-front** testing of materials, components and systems.
- Accelerated degradation tests can be useful for such **up-front** testing.

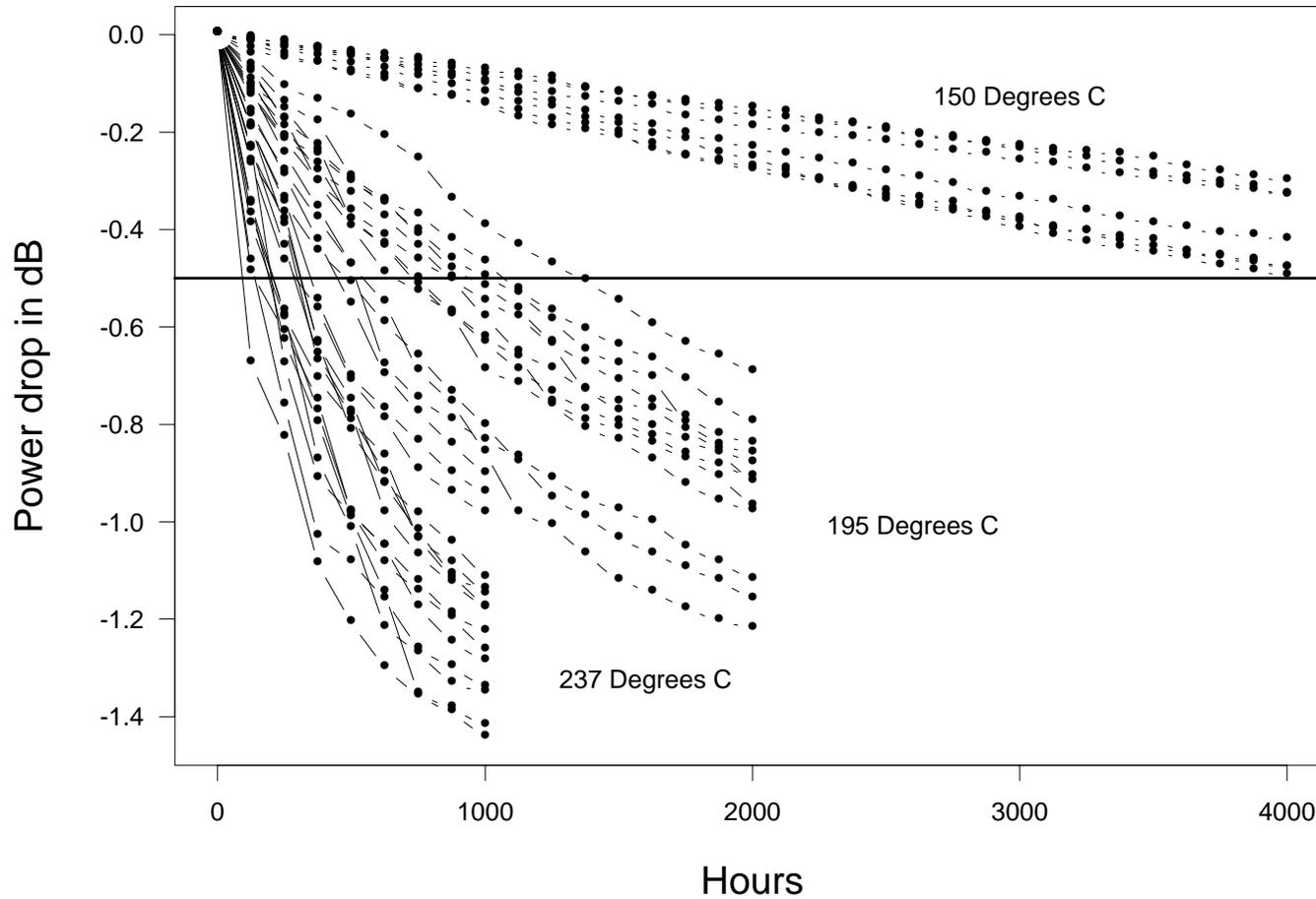
# Percent Increase in Resistance Over Time for Carbon-Film Resistors (Shiomi and Yanagisawa 1979)



## Advantages of Using Degradation Data Over Failure-Time Data

- Degradation is natural response for some tests.
- Useful reliability inferences even with 0 failures.
- More justification and credibility for extrapolative acceleration models.  
(Modeling closer to physics-of-failure)
- Can be more informative than failure-time data.  
(Reduction to failure-time data loses information)

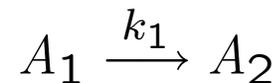
# Device-B Power Drop Accelerated Degradation Test Results at 150°C, 195°C, and 237°C (Use Conditions 80°C)



## Device-B Power Drop

### Simple One-Step Chemical Reaction Leading to Failure

- $A_1(t)$  is the amount of harmful material available for reaction at time  $t$
- $A_2(t)$  is proportional to the amount of failure-causing compounds at time  $t$ .
- Chemical reaction:



- Power drop proportional to  $A_2(t)$
- The rate equations for this reaction are

$$\frac{dA_1}{dt} = -k_1 A_1 \quad \text{and} \quad \frac{dA_2}{dt} = k_1 A_1$$

## Device-B Power Drop Simple One-Step Chemical Reaction Leading to Failure (continued)

- Solution to differential equations:

$$A_1(t) = A_1(0) \exp(-k_1 t)$$

$$A_2(t) = A_2(0) + A_1(0)[1 - \exp(-k_1 t)]$$

where  $A_1(0)$  and  $A_2(0)$  are initial conditions.

- If  $A_2(0) = 0$ , then  $\mathcal{D}_\infty = \lim_{t \rightarrow \infty} A_2(t) = A_1(0)$  and the solution for  $A_2(t)$  (the function of primary interest) can be reexpressed as

$$A_2(t) = A_1(t)[1 - \exp(-k_1 t)]$$

$$\mathcal{D}(t) = \mathcal{D}_\infty [1 - \exp(-\mathcal{R} t)]$$

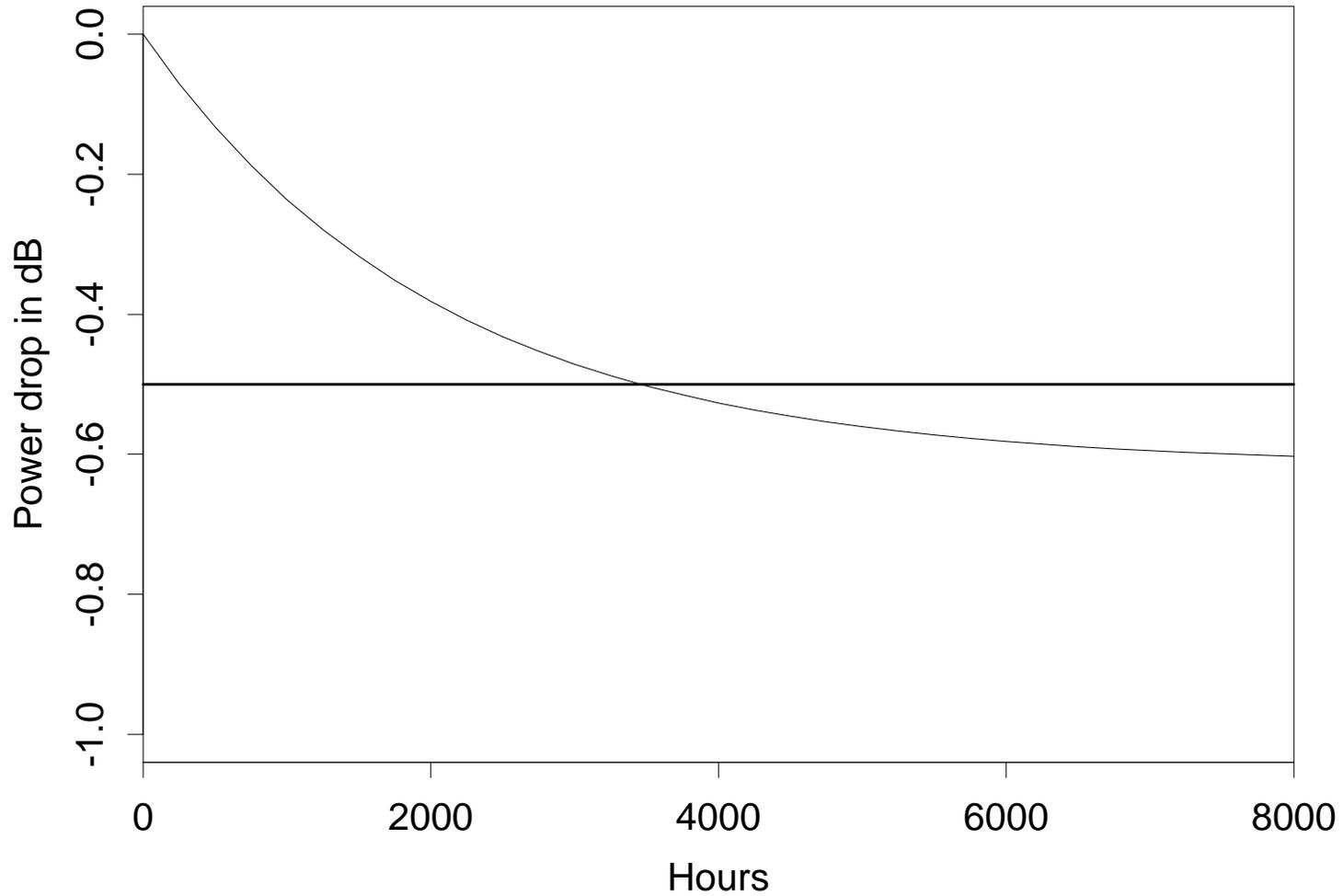
where  $\mathcal{D}(t) = A_2(t)$  is the degradation at time  $t$  and  $\mathcal{R} = k_1$  is the reaction rate.

- A simple 1-step diffusion process has the same solution.

# Device-B Power Drop

$$\mathcal{D}(t) = \mathcal{D}_\infty [1 - \exp(-\mathcal{R}t)]$$

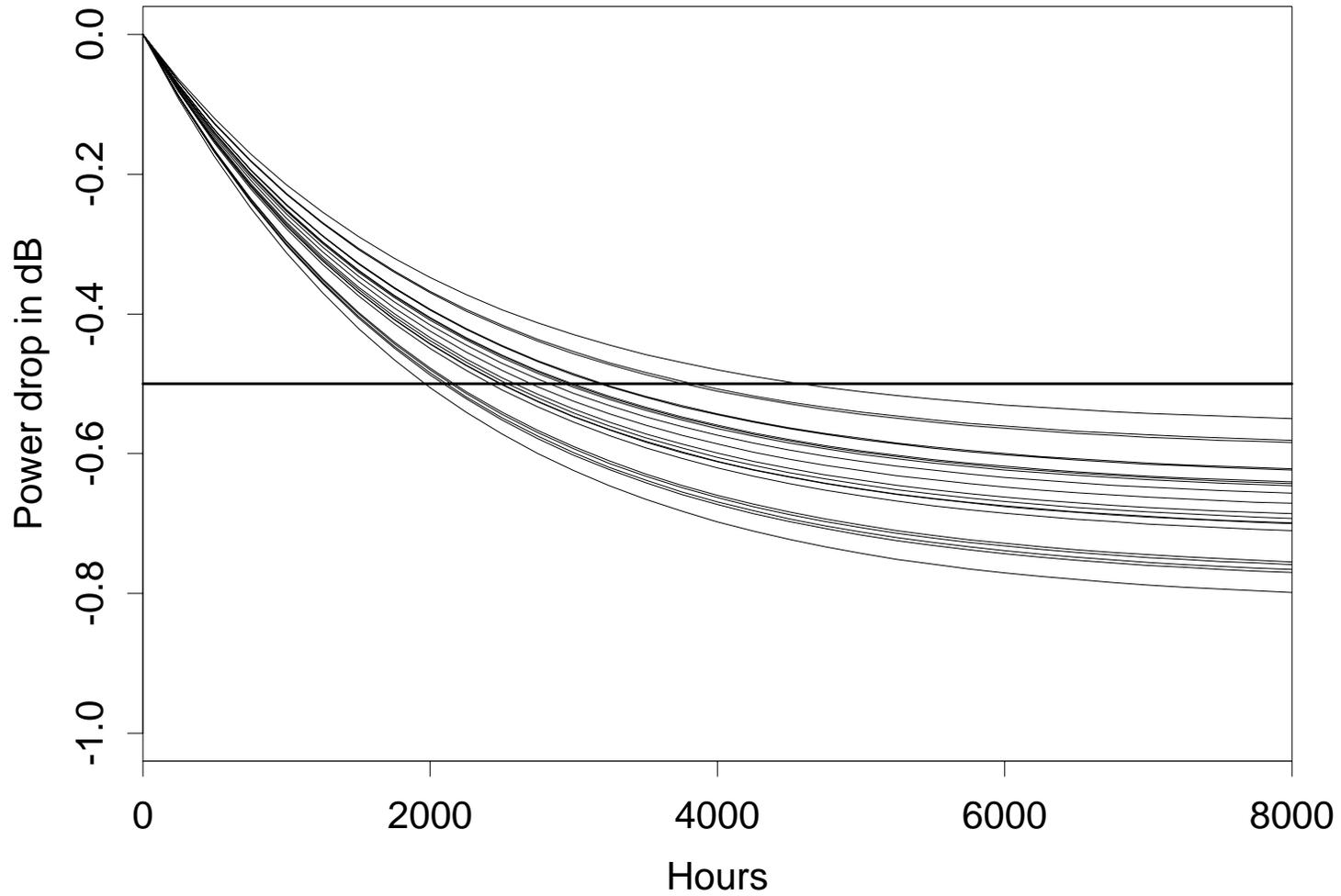
Fixed  $\mathcal{D}_\infty$  and Rate  $\mathcal{R}$



# Device-B Power Drop

$$D(t) = D_{\infty}[1 - \exp(-\mathcal{R}t)]$$

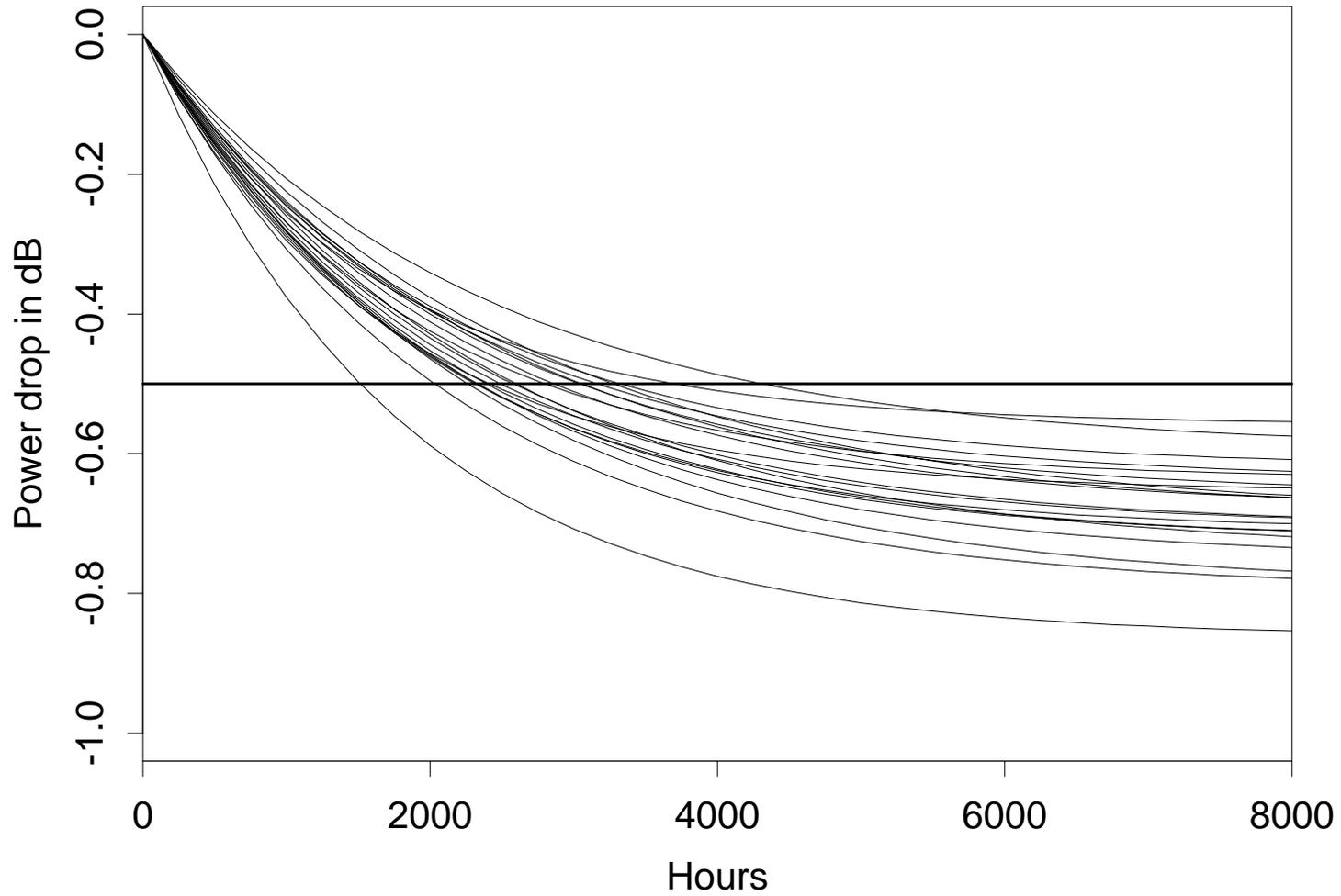
Variability in Asymptote  $D_{\infty}$



# Device-B Power Drop

$$D(t) = D_{\infty}[1 - \exp(-\mathcal{R}t)]$$

Variability in Asymptote  $D_{\infty}$  and Rate  $\mathcal{R}$



## Model for Degradation Data

- **Actual degradation path model:** Actual path of unit  $i$ th at time  $t_{ij}$  is

$$D_{ij} = \mathcal{D}(t_{ij}, \beta_{1i}, \dots, \beta_{ki})$$

- **Path parameters:**  $\beta_{1i}, \dots, \beta_{ki}$  may be random from unit-to-unit or fixed in the population/process.

- **Sample path model:** Sample degradation path of unit  $i$ th at  $t_{ij}$  (the  $j$ th inspection time for unit  $i$ ) is

$$y_{ij} = D_{ij} + \epsilon_{ij}, \quad \epsilon_{ij} \sim \text{NID}(0, \sigma_\epsilon^2), \quad i = 1, \dots, n, \quad j = 1, \dots, m_i.$$

- Can use transformations on the response, time, or random parameters, as suggested by physical/chemical theory, past experience, or the data.

## Acceleration of Degradation

- The **Arrhenius** model describing the effect that temperature has on the **rate** of a simple one-step chemical reaction is

$$\mathcal{R}(\text{temp}) = \gamma_0 \exp\left(\frac{-E_a}{k_B(\text{temp} + 273.15)}\right)$$

where temp is temperature in °C and  $k_B = 8.6 \times 10^{-5}$  is Boltzmann's constant in units of electron volts per °C.

- The pre-exponential factor  $\gamma_0$  and the reaction activation energy  $E_a$  are characteristics of the product or material.
- The **Acceleration Factor** between temp and  $\text{temp}_U$  is

$$\mathcal{AF}(\text{temp}) = \mathcal{AF}(\text{temp}, \text{temp}_U, E_a) = \frac{\mathcal{R}(\text{temp})}{\mathcal{R}(\text{temp}_U)}$$

When  $\text{temp} > \text{temp}_U$ ,  $\mathcal{AF}(\text{temp}, \text{temp}_U, E_a) > 1$ .

## Arrhenius Model Temperature Effect on Time to an Event

- Re-expressing the single-step chemical reaction degradation path model to allow for acceleration:

$$\mathcal{D}(t; \text{temp}) = \mathcal{D}_{\infty} \times \{1 - \exp[-\{\mathcal{R}_U \times \mathcal{AF}(\text{temp})\} \times t]\}$$

where  $\mathcal{R}_U$  is the rate reaction at  $\text{temp}_U$ .

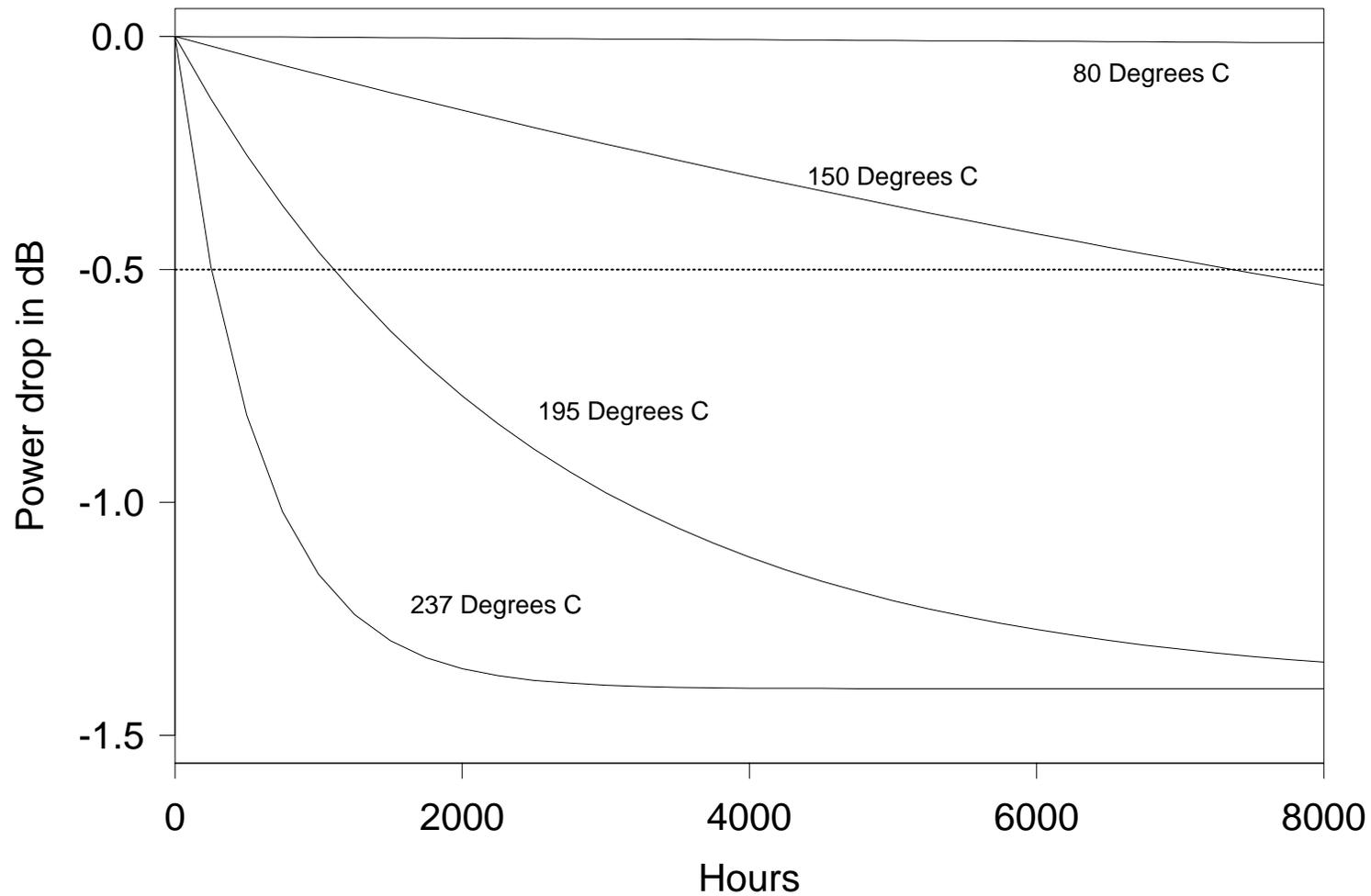
- Failure defined by  $\mathcal{D}(t) < \mathcal{D}_f$ .
- Equating  $\mathcal{D}(T; \text{temp})$  to  $\mathcal{D}_f$  and solving for  $T$  gives the failure time at temperature  $\text{temp}$  as

$$T(\text{temp}) = \frac{\left[-\frac{1}{\mathcal{R}_U} \log\left(1 - \frac{\mathcal{D}_f}{\mathcal{D}_{\infty}}\right)\right]}{\mathcal{AF}(\text{temp})} = \frac{T(\text{temp}_U)}{\mathcal{AF}(\text{temp})}$$

- Thus the simple degradation process induces a Scale Accelerated Failure Time (SAFT) model.

# Illustration of the Effect of Arrhenius Temperature Dependence on the Degradation Caused by a Single-Step Chemical Reaction

$$D(t; \text{temp}) = D_{\infty} \times \{1 - \exp[-\{\mathcal{R}_U \times \mathcal{AF}(\text{temp})\} \times t]\}$$



## Device-B Power Drop Degradation Model and Parameters

- **Basic parameters:**  $\mathcal{R}_U = \mathcal{R}(80)$ ,  $\mathcal{D}_\infty$ ,  $E_a$ .
- **Estimation parameters:**  
 $\beta_1 = \log[\mathcal{R}(195)]$ ,  $\beta_2 = \log(-\mathcal{D}_\infty)$ , and  $\beta_3 = E_a$ .
- Assume that  $(\beta_1, \beta_2)$  follow a bivariate normal distribution.
- Assume that activation energy  $\beta_3 = E_a$  is a fixed (but unknown) characteristic of Device-B.
- **Variability in path model parameters:**  $(\beta_1, \beta_2, \beta_3) \sim \text{MVN}(\mu_\beta, \Sigma_\beta)$   
[but  $\text{Var}(\beta_3)=0$ ].

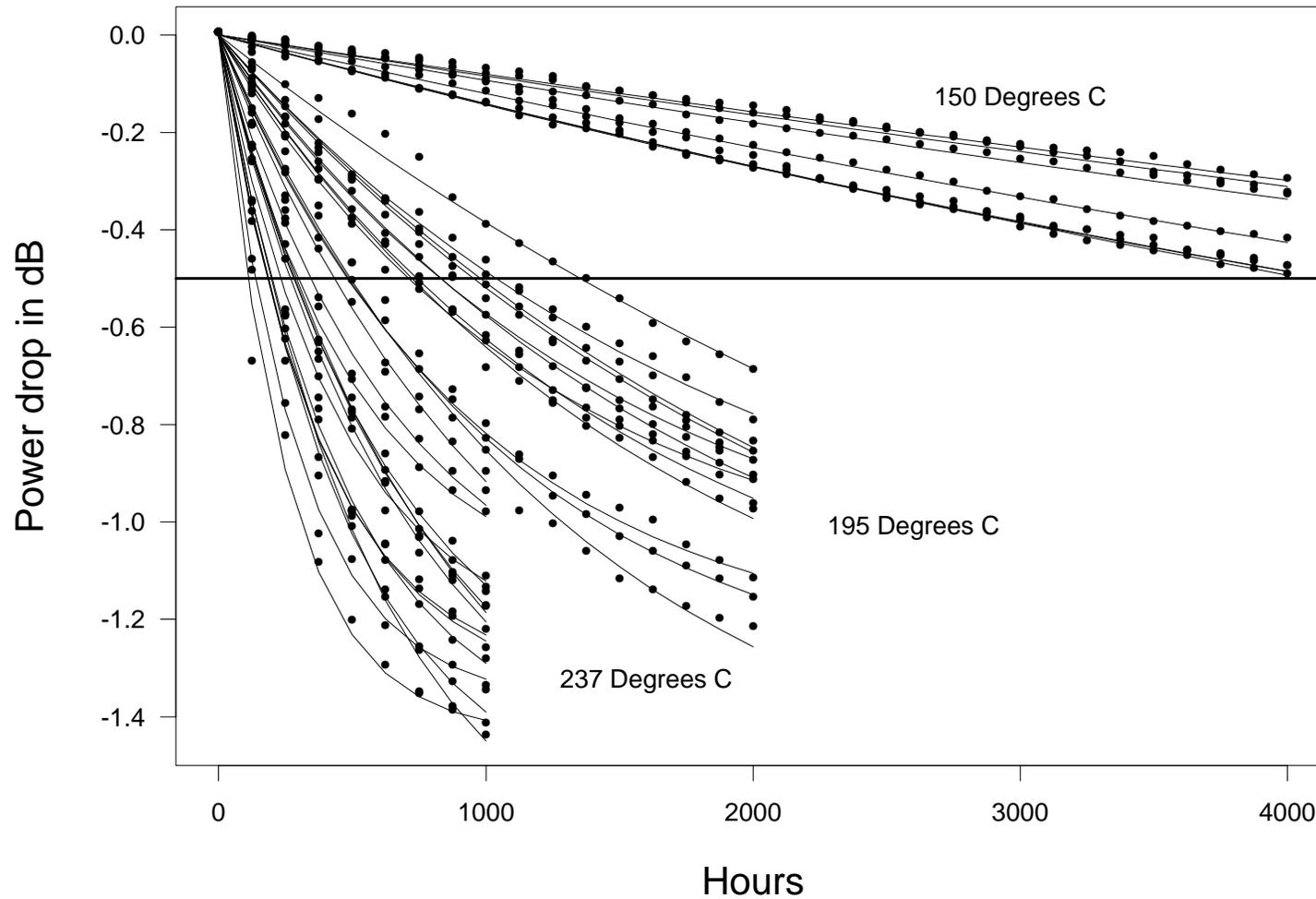
**Device-B Power Drop Data**  
**Approximate ML Estimates**  
**(Computed with Program of Pinheiro and Bates 1995)**

$$\hat{\mu}_{\beta} = \begin{pmatrix} -7.572 \\ .3510 \\ .6670 \end{pmatrix}, \quad \hat{\Sigma}_{\beta} = \begin{pmatrix} .15021 & -.02918 & 0 \\ -.02918 & .01809 & 0 \\ 0 & 0 & 0 \end{pmatrix},$$

$$\hat{\sigma}_{\epsilon} = .0233,$$

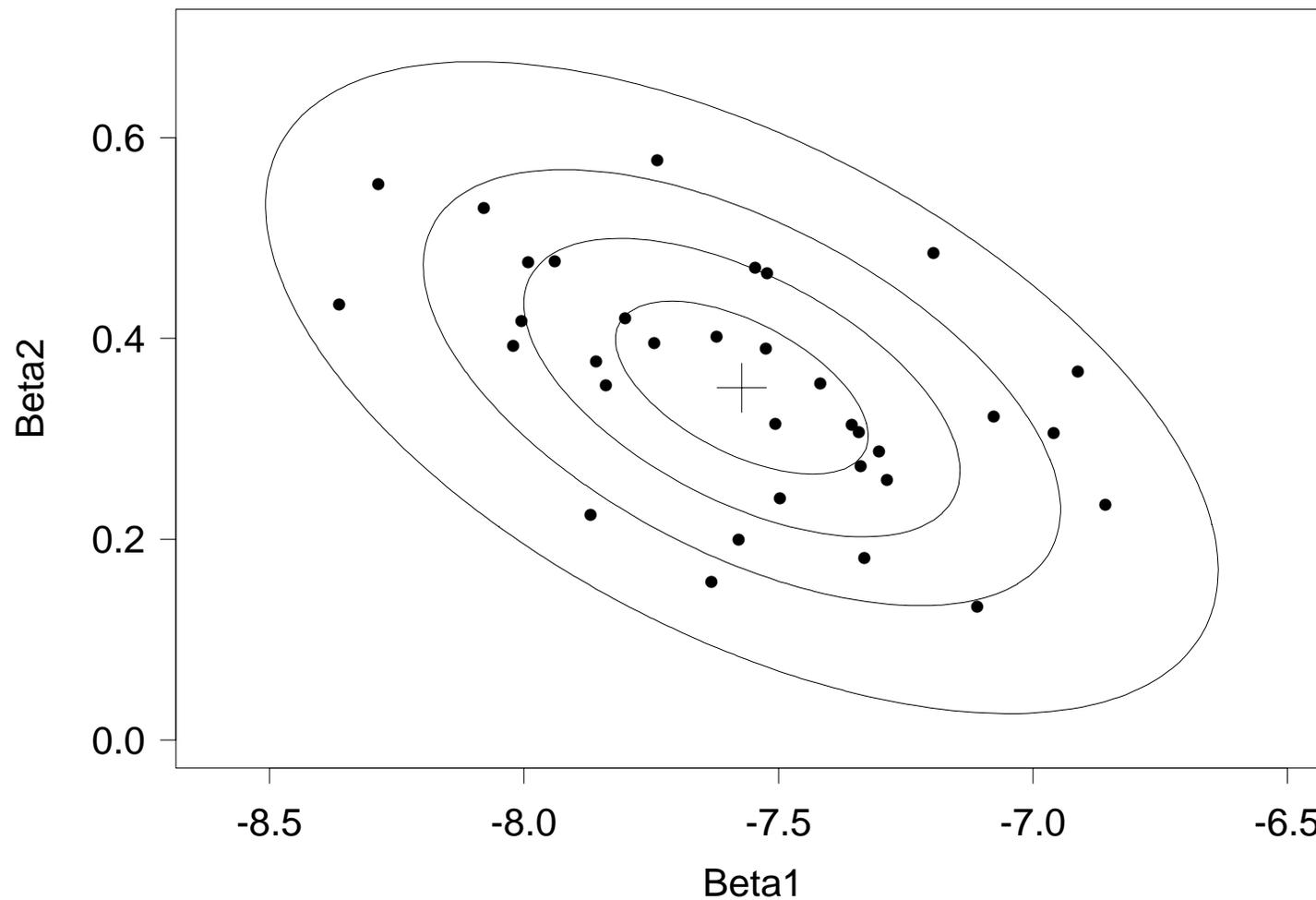
Loglikelihood = 1201.8.

# Device-B Power Drop Observations and Fitted Degradation Model for the $i = 1, \dots, 34$ Sample Paths



**Plot of  $\beta_1 = \log[\mathcal{R}(195)]$  Versus  $\beta_2 = \log(-\mathcal{D}_\infty)$   
for the  $i = 1, \dots, 34$  Sample Paths from Device-B**

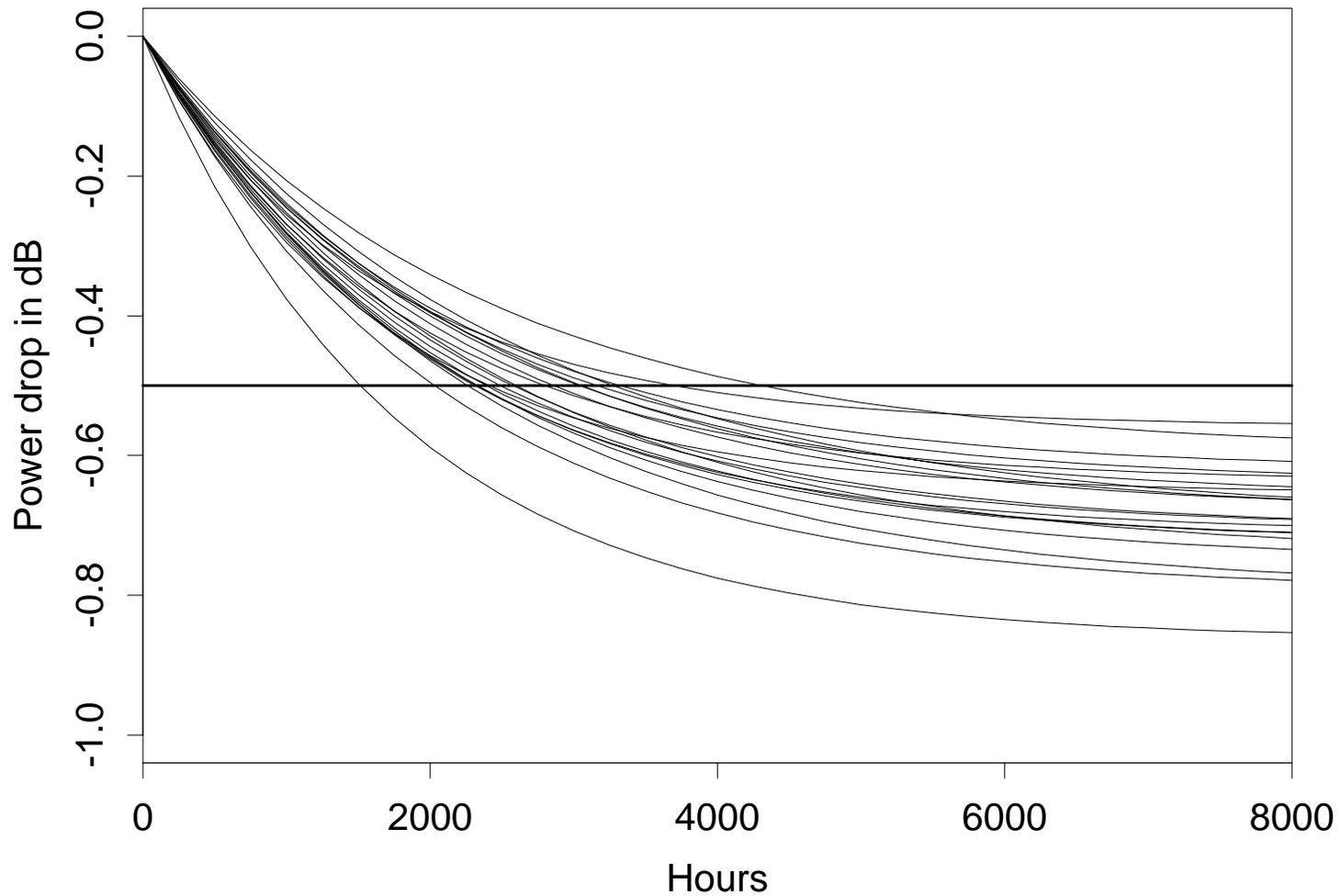
$$\hat{\rho}_{\beta_1\beta_2} = -.56$$



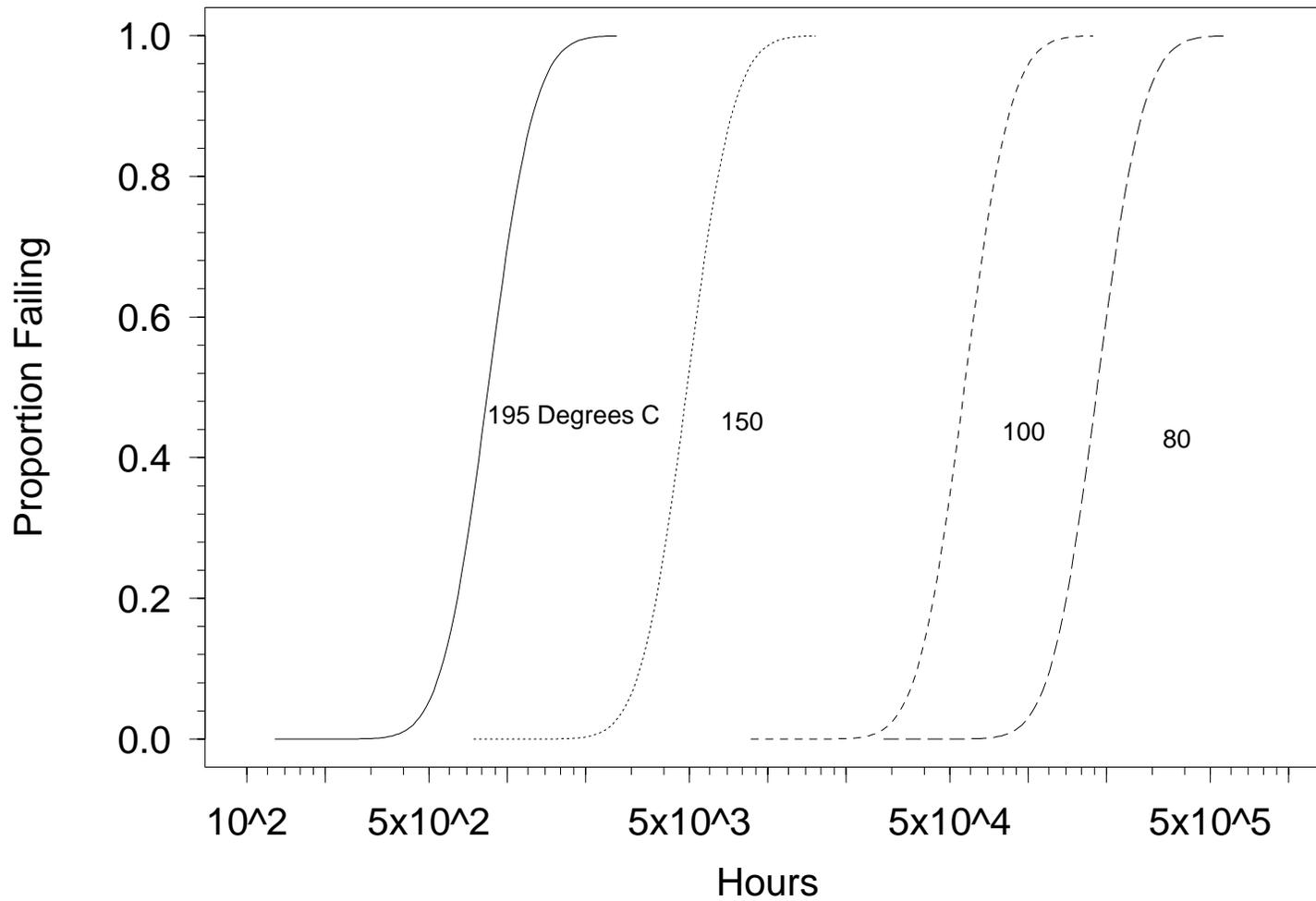
# Device-B Power Drop

$$\mathcal{D}(t) = \mathcal{D}_\infty [1 - \exp(-\mathcal{R}t)]$$

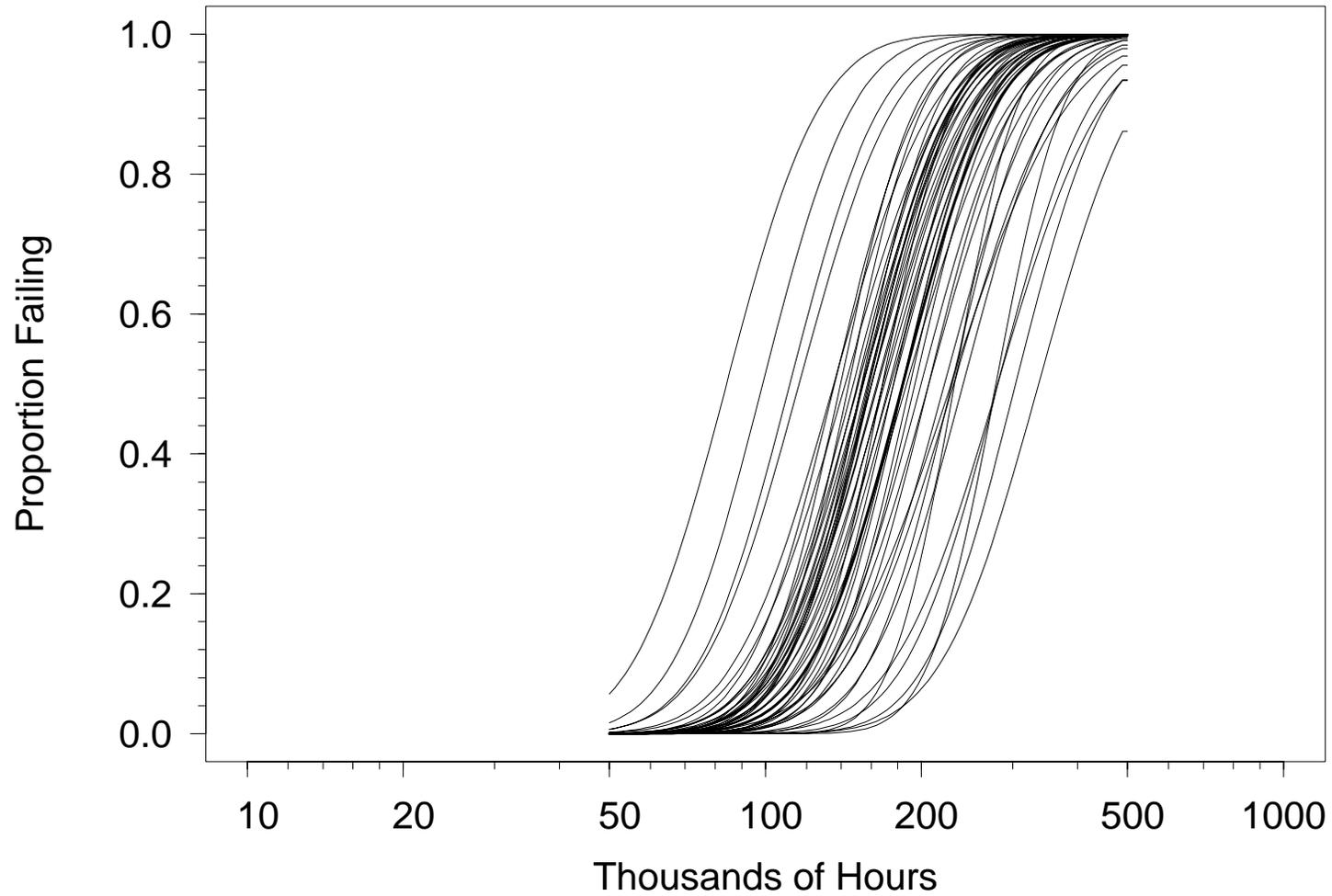
Variability in Asymptote  $\mathcal{D}_\infty$  and rate  $\mathcal{R}$



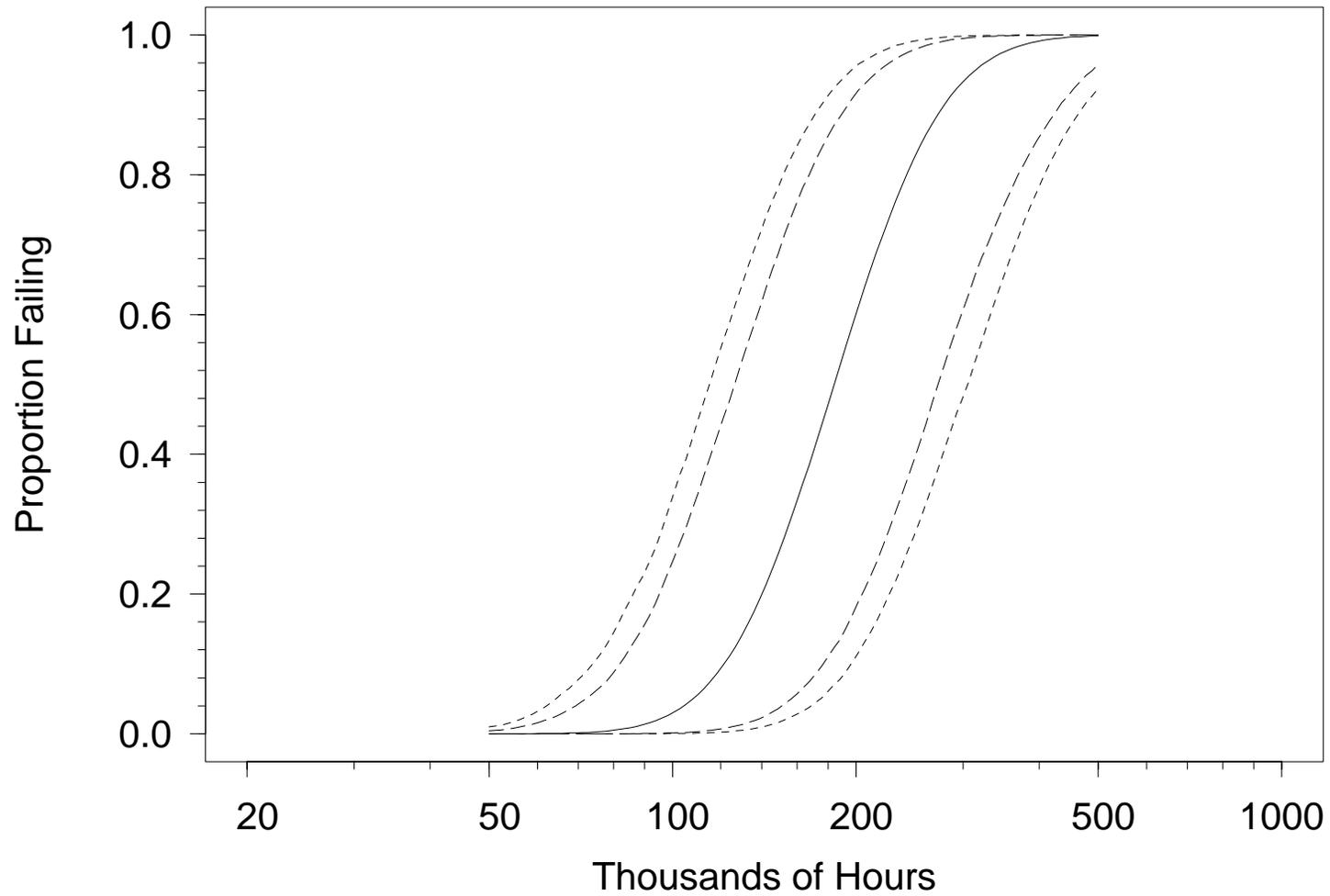
# Estimates of the Device-B Life Distributions at 80, 100, 150, and 190°C, Based on the Degradation Data



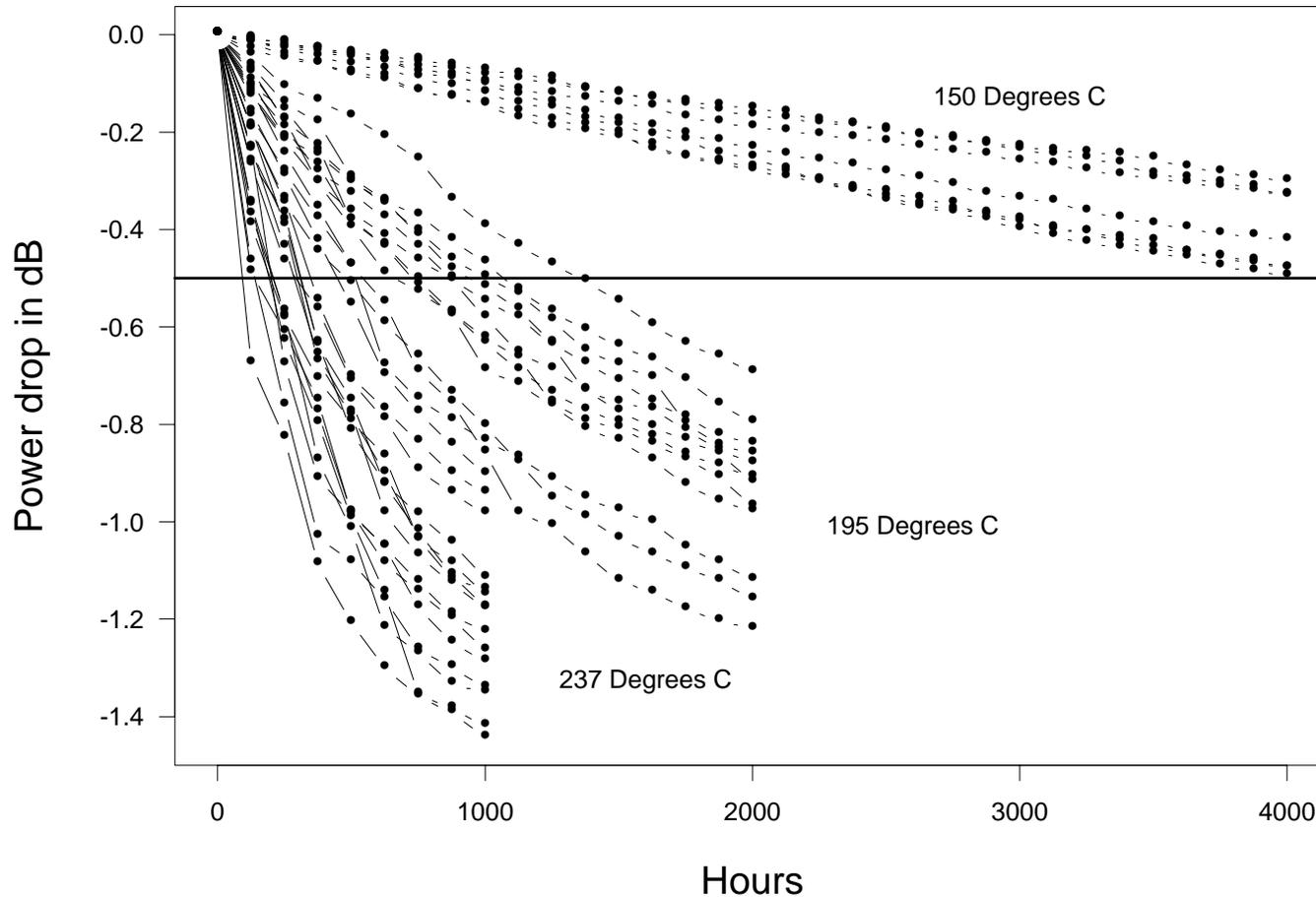
# Bootstrap Sample Estimates of $F(t)$ at 80°C



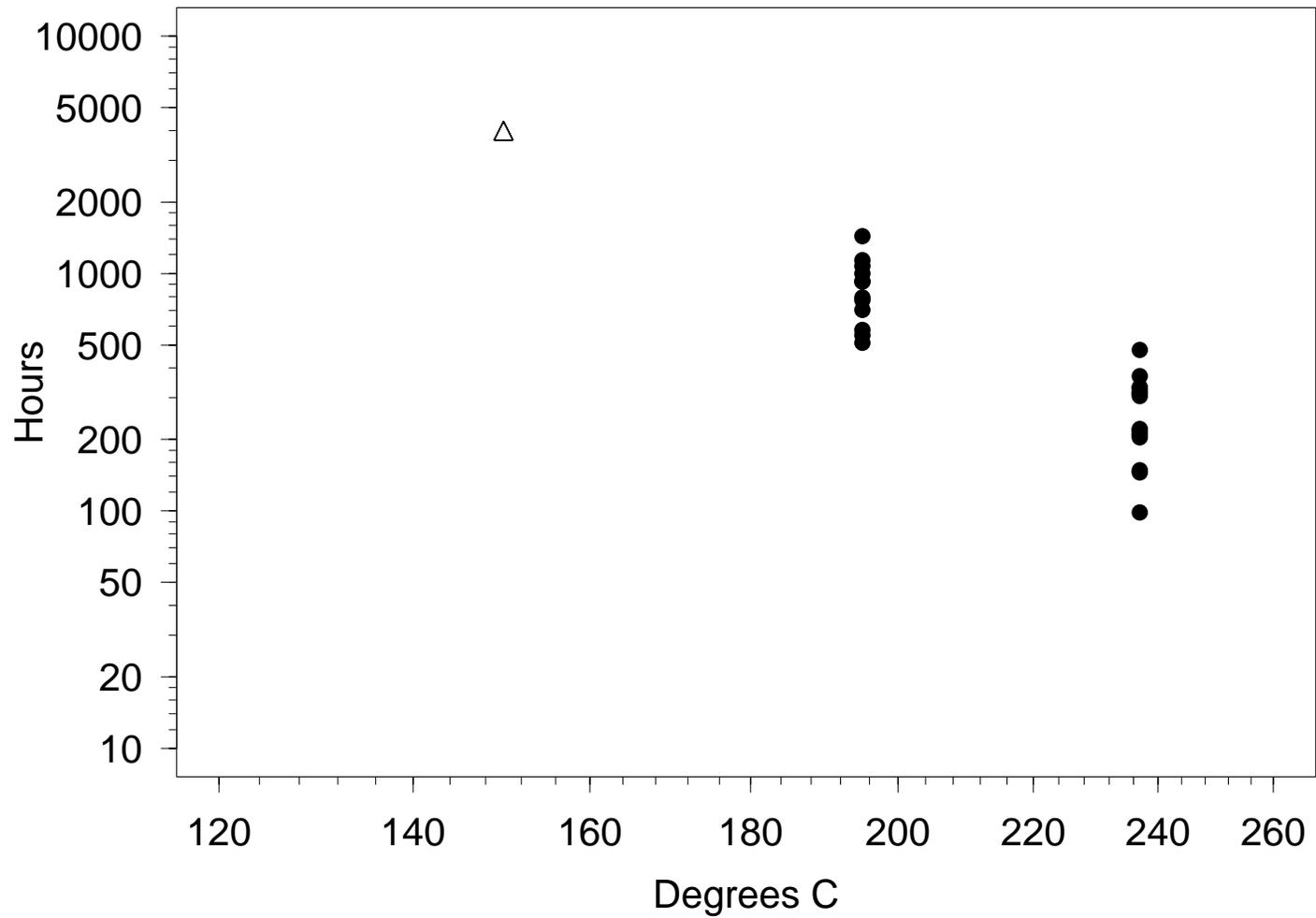
# 80% and 90% Bias-Corrected Percentile Bootstrap Confidence Intervals for $F(t)$ at 80°C



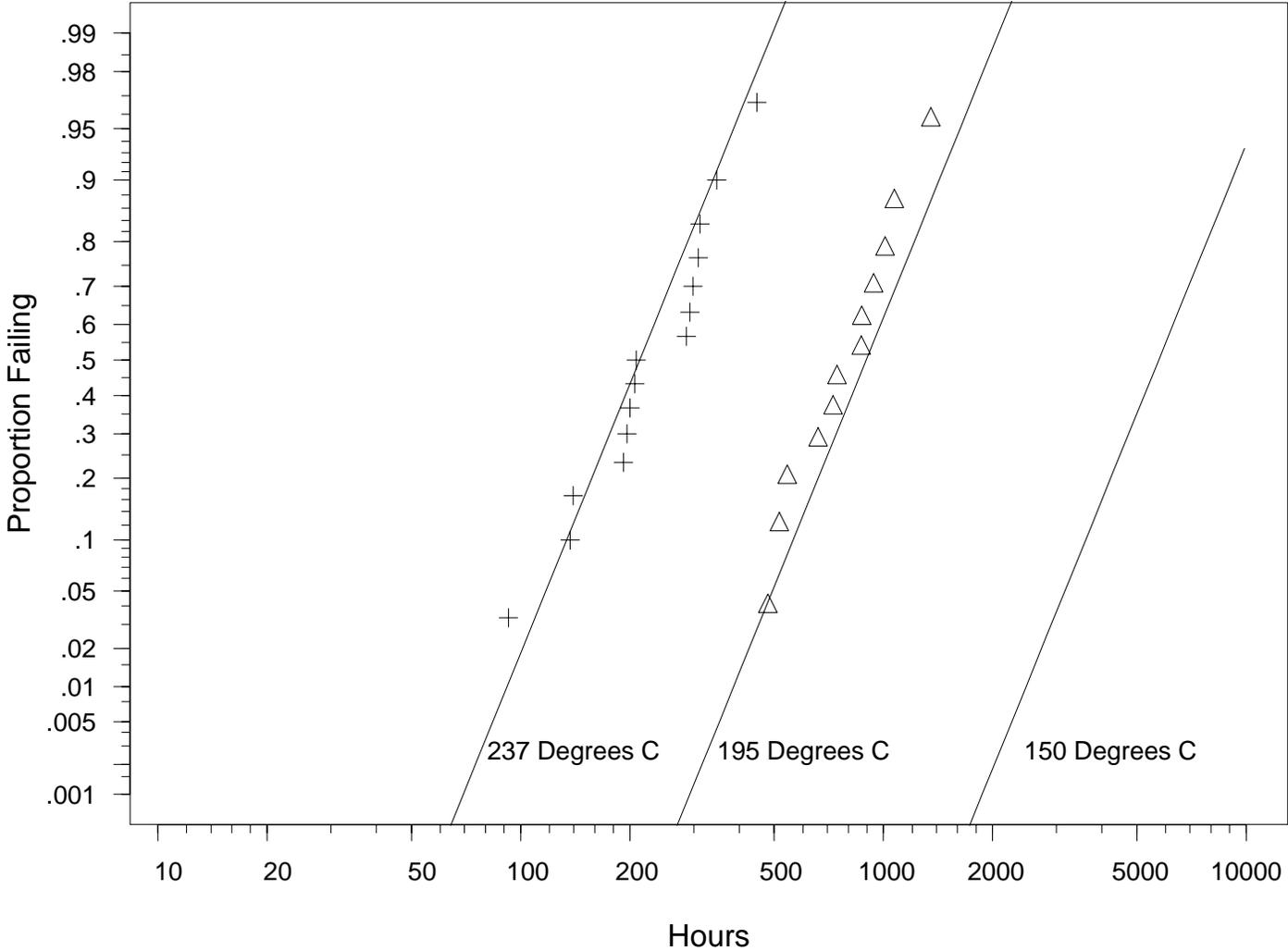
# Device-B Power Drop Accelerated Degradation Test Results at 150°C, 195°C, and 237°C (Use Conditions 80°C)



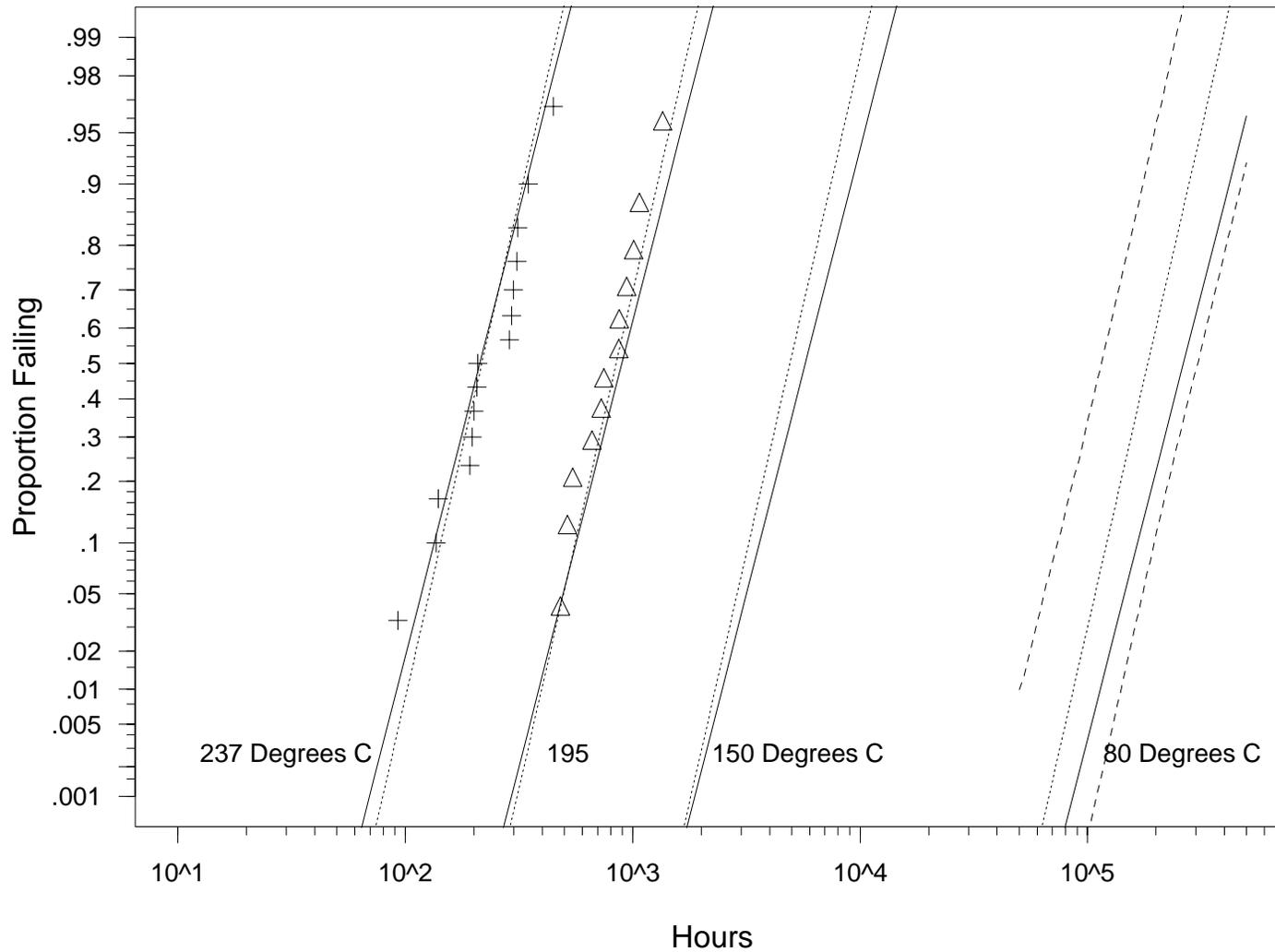
# Scatterplot of Device-B Failure-Time Data with Failure Defined as Power Drop Below $-0.5$ dB



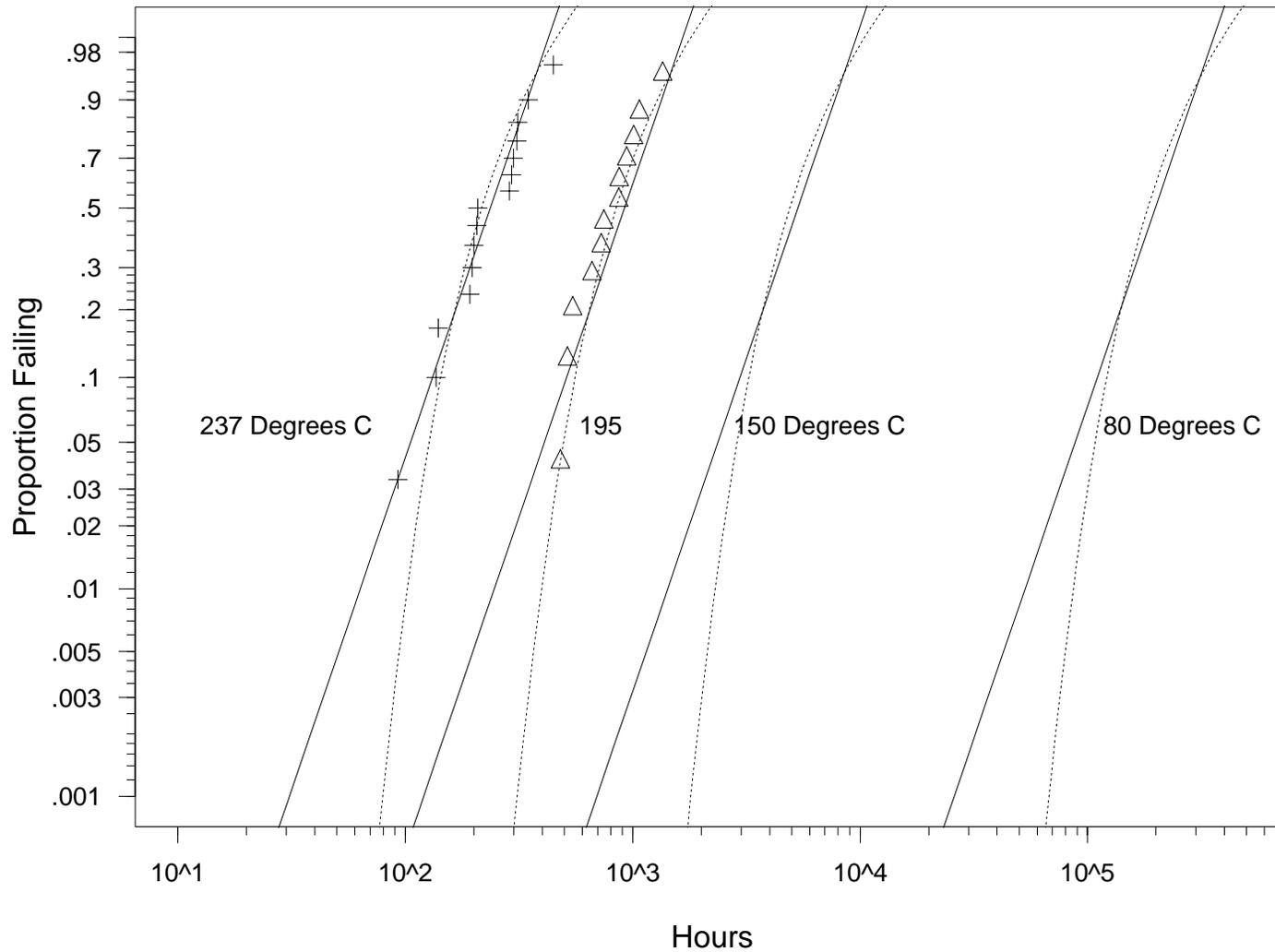
# Lognormal-Arrhenius Model Fit to the Device-B Failure-Time Data



# Lognormal-Arrhenius Model Fit to the Device-B Failure-Time Data with Degradation Model Estimates

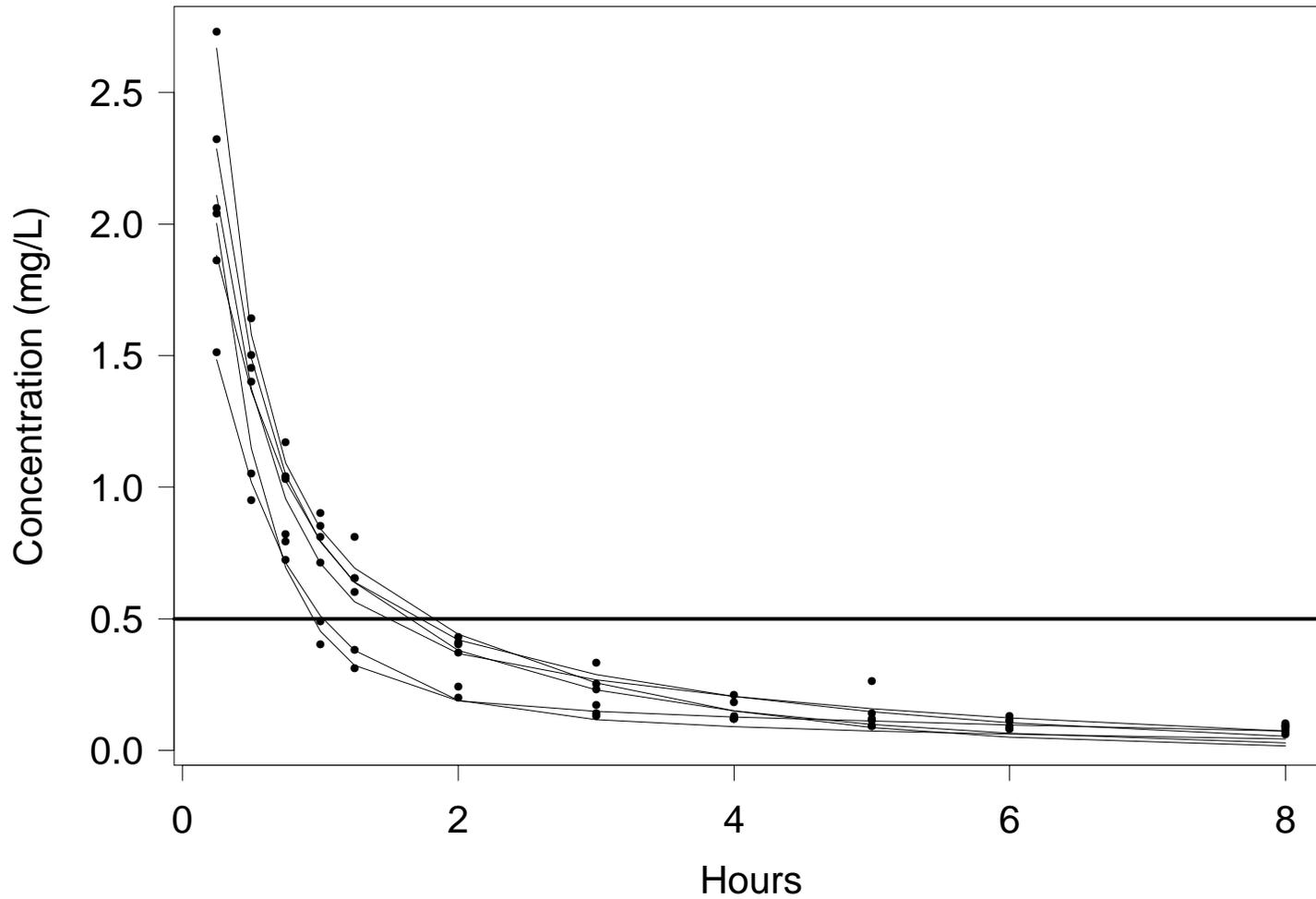


# Weibull-Arrhenius Model Fit to the Device-B Failure-Time Data with Degradation Model Estimates



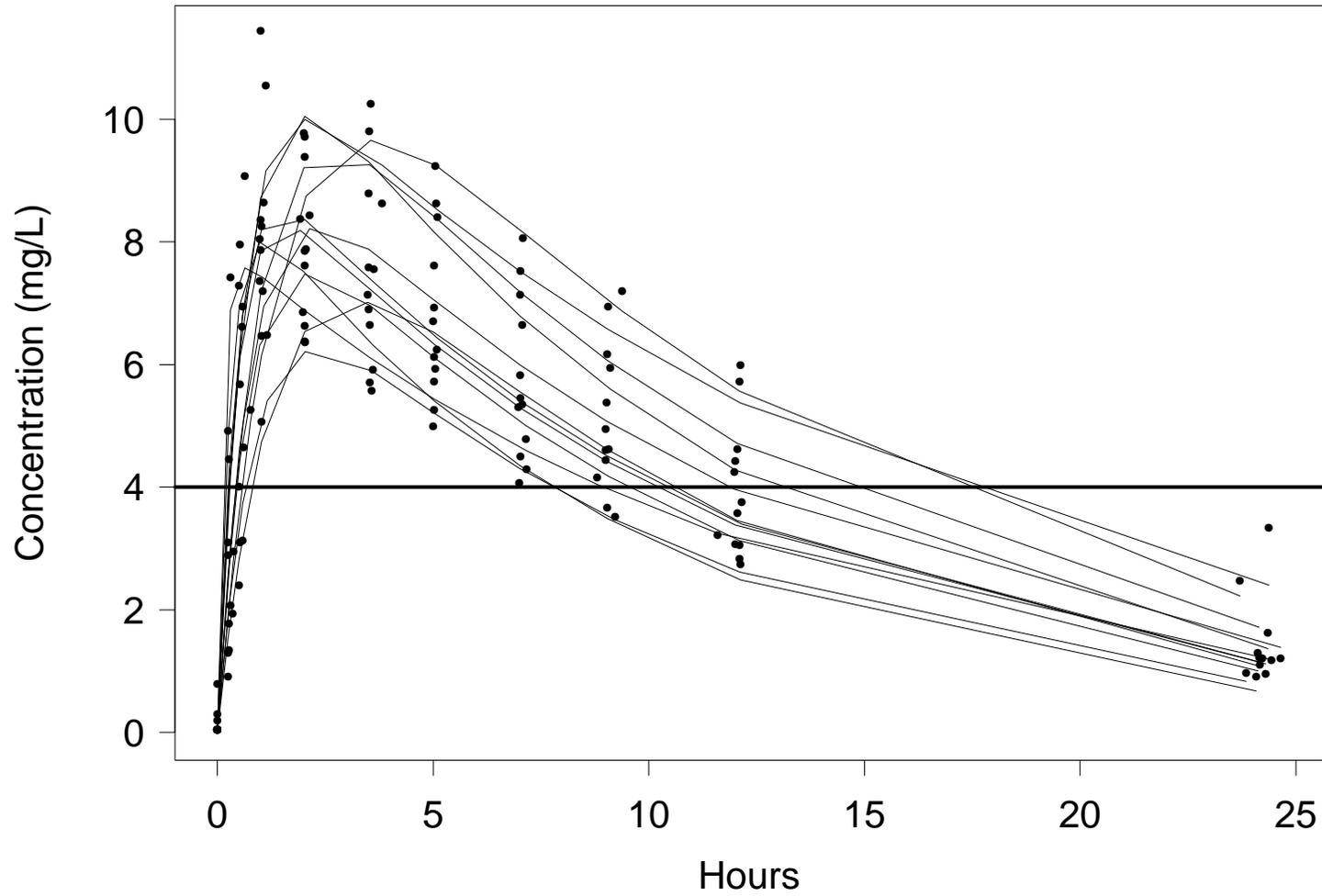
# Plasma Concentrations of Indomethacin Following Intravenous Injection

## Fitted Biexponential Model



# Theophylline Serum Concentrations

## Fitted Curves for a First-Order Compartment Model



## Approximate Accelerated Degradation Analysis

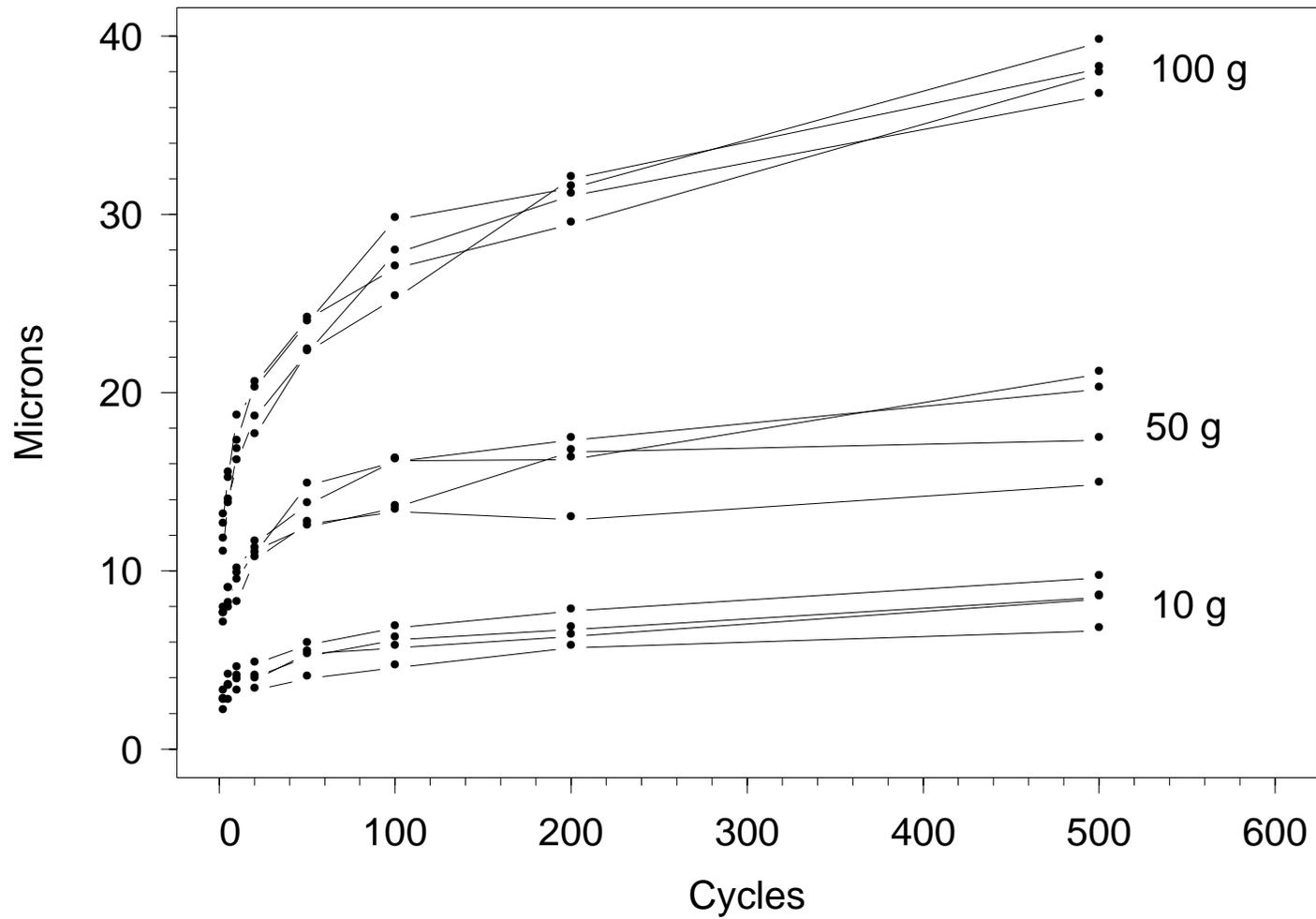
The simple method for degradation data analysis extends directly to accelerated degradation analysis.

- For each sample path one uses the algorithm described to predict the failure times.
- These data can be analyzed using the methods to analyze ALT data.
- It is important to remember, however, that such an analysis has the same limitations described in for the simple analysis of degradation data.

## Sliding Metal Wear Data Analysis

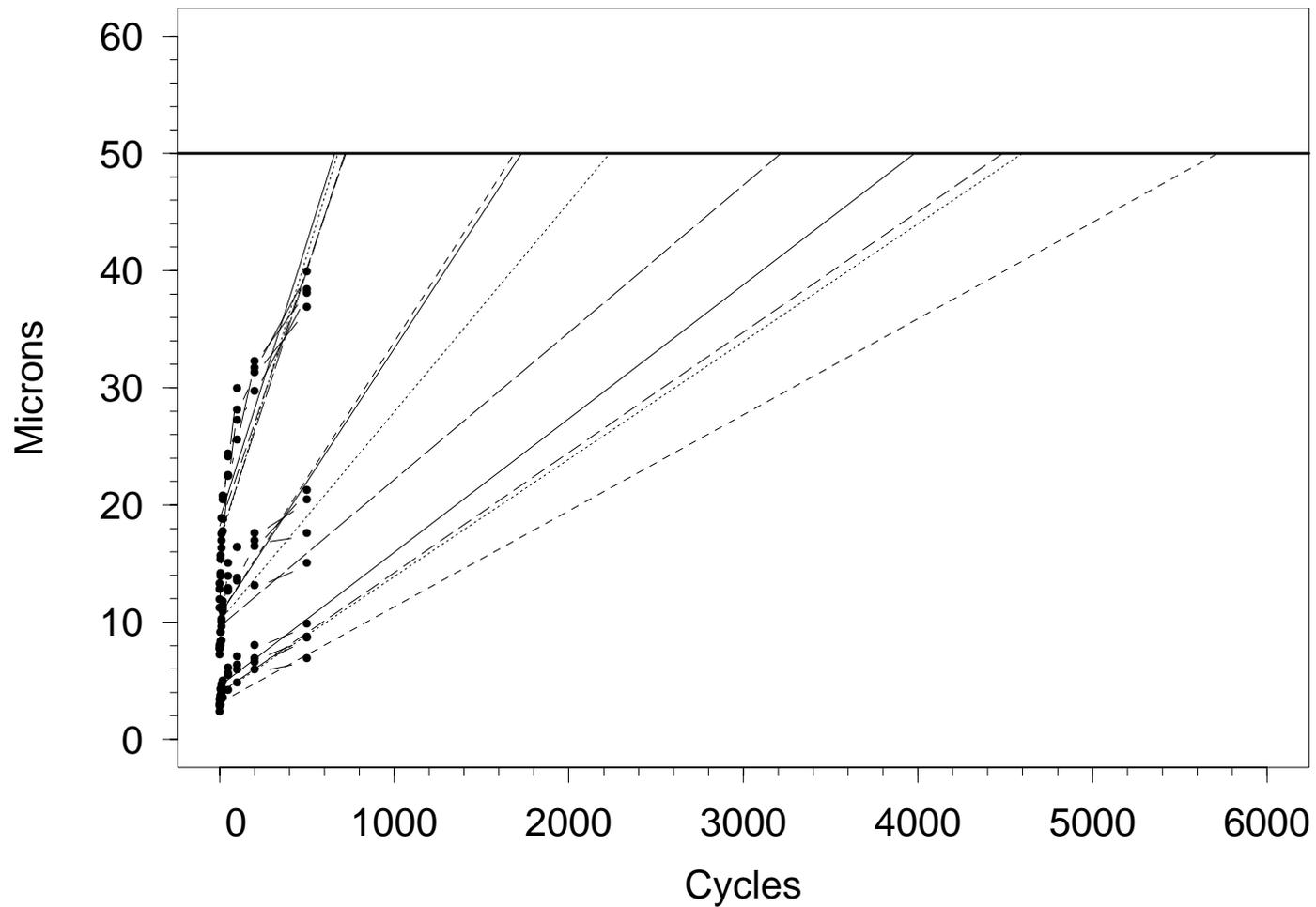
- An experiment was conducted to test the wear resistance of a particular metal alloy.
- The sliding test was conducted over a range of different applied weights in order to study the effect of weight and to gain a better understanding of the wear mechanism.
- The predicted pseudo failure times were obtained by using ordinary least squares to fit a line through each sample path on the log-log scale and extrapolating to the time at which the scar width would be 50 microns.

# Scar Width Resulting from a Metal-to-Metal Sliding Test for Different Applied Weights

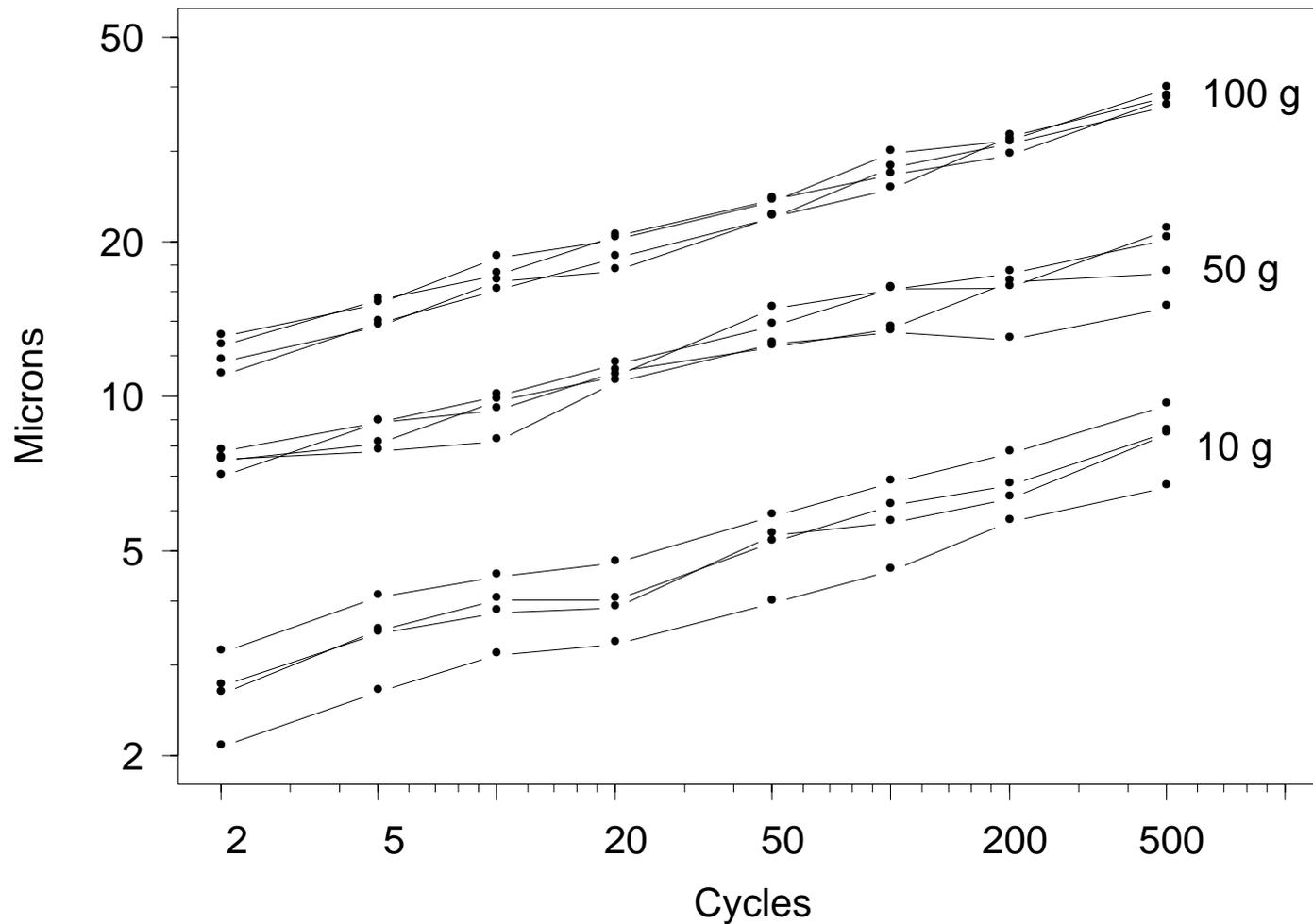


# Metal-to-Metal Sliding Test for Different Applied Weights

Extrapolation to Failure Definition  
(Using linear regression on linear axes)

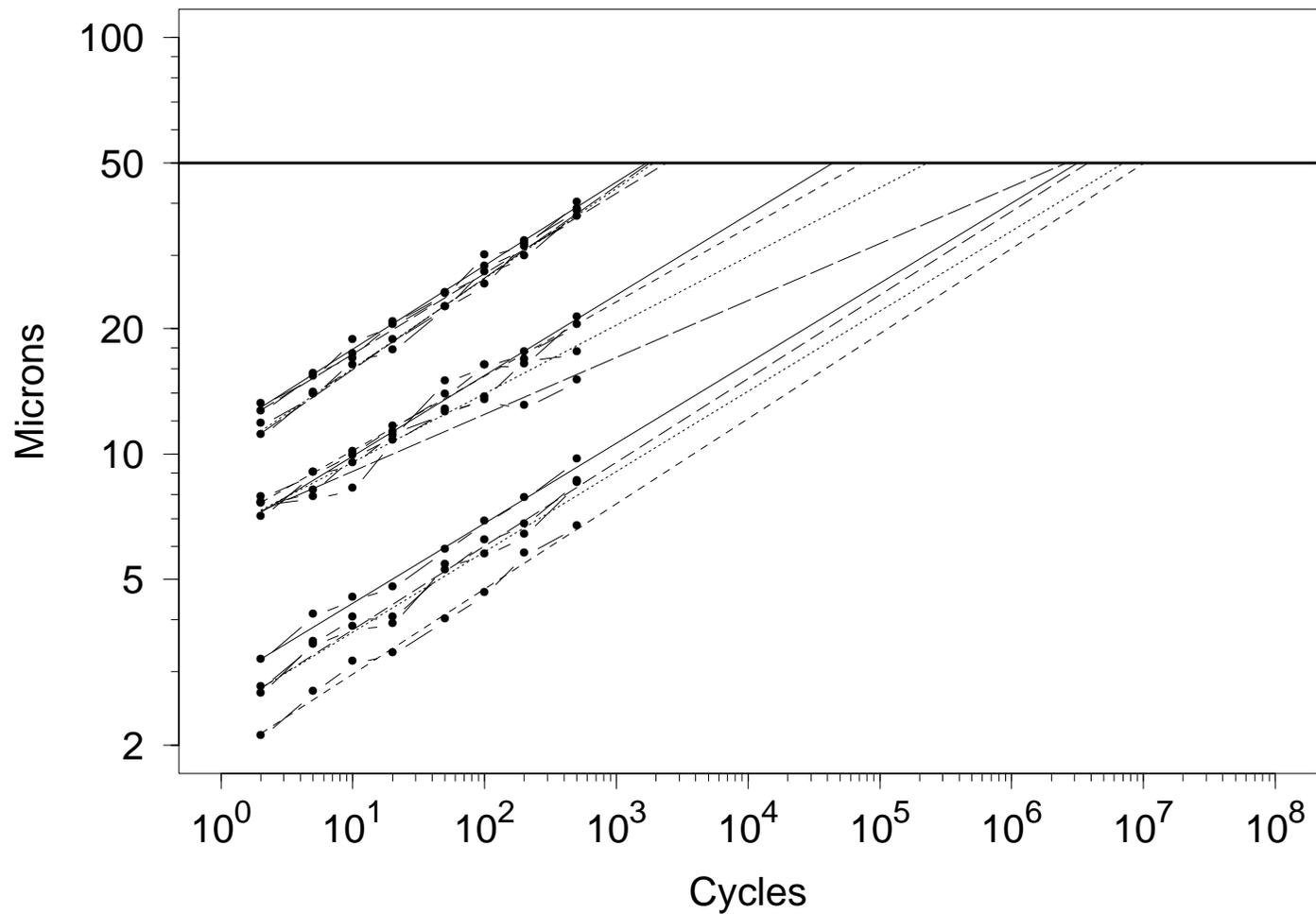


# Scar Width Resulting from a Metal-to-Metal Sliding Test for Different Applied Weights (Using log-log Axes)



# Metal-to-Metal Sliding Test for Different Applied Weights

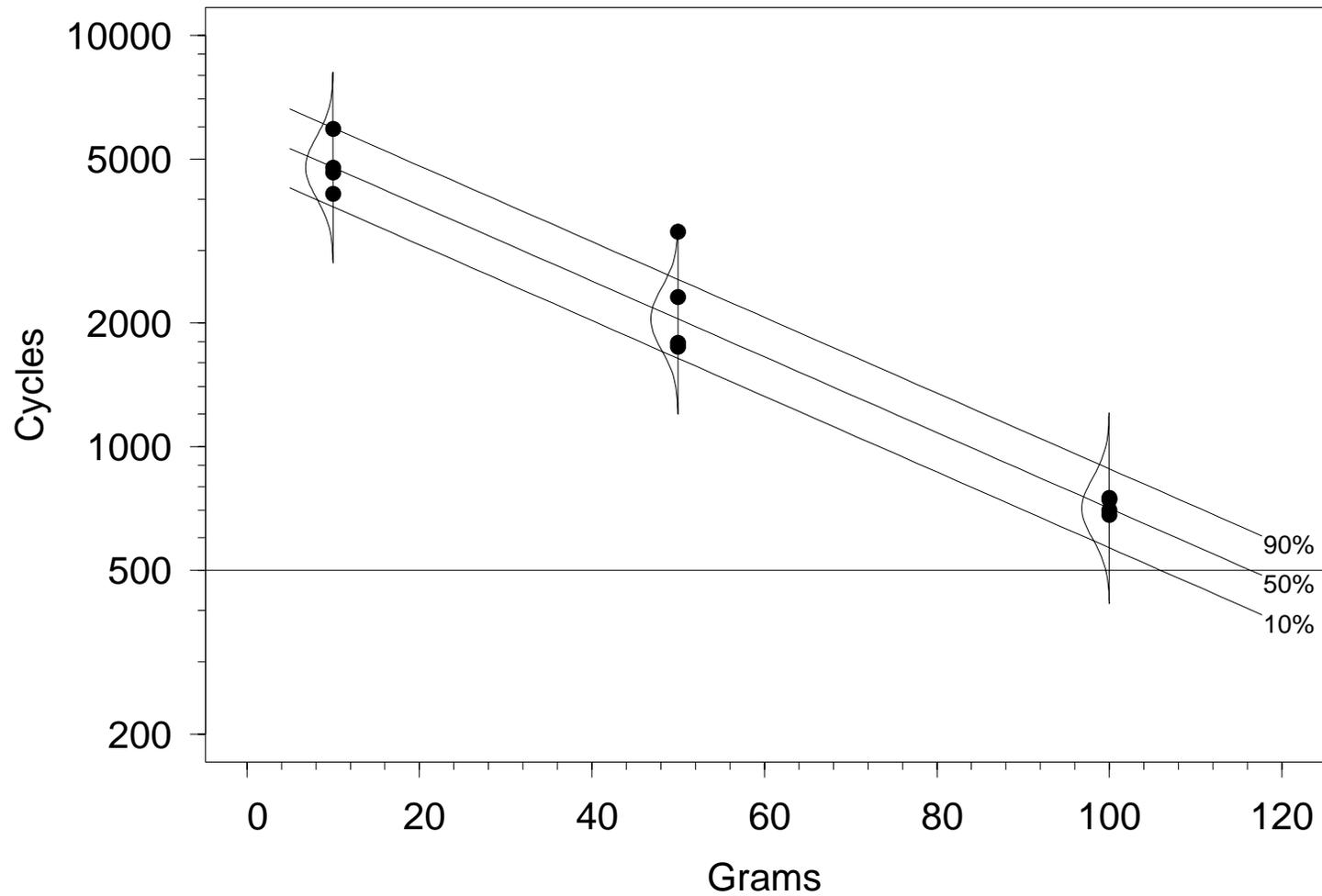
Extrapolation to Failure Definition  
(Using linear regression on log-log axes)



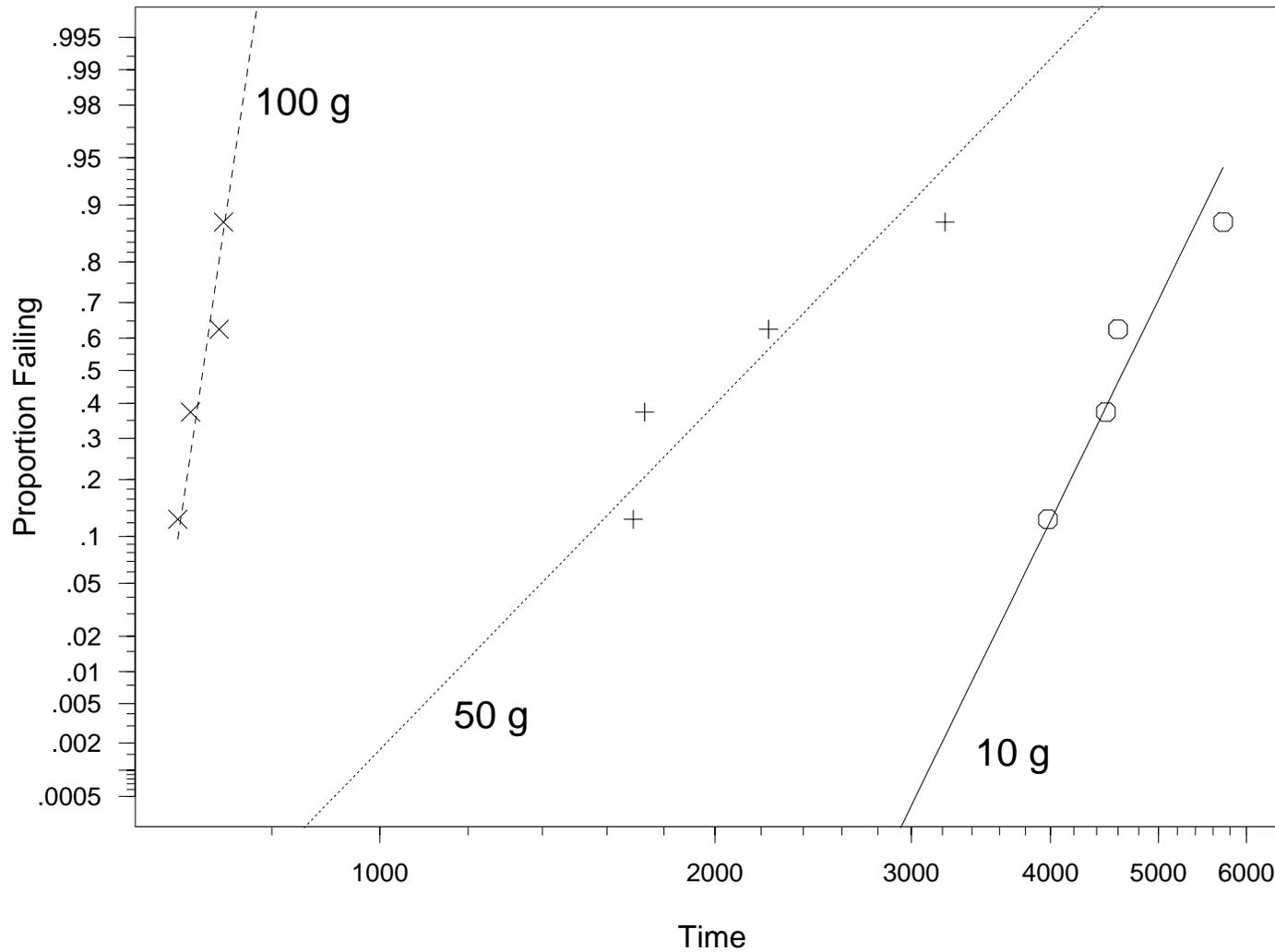
## Metal-Wear Failure Times in Hours

Grams	Pseudo Failure Times			
100	724	718	659	677
50	3216	1729	2234	1689
10	3981	4600	5718	4487

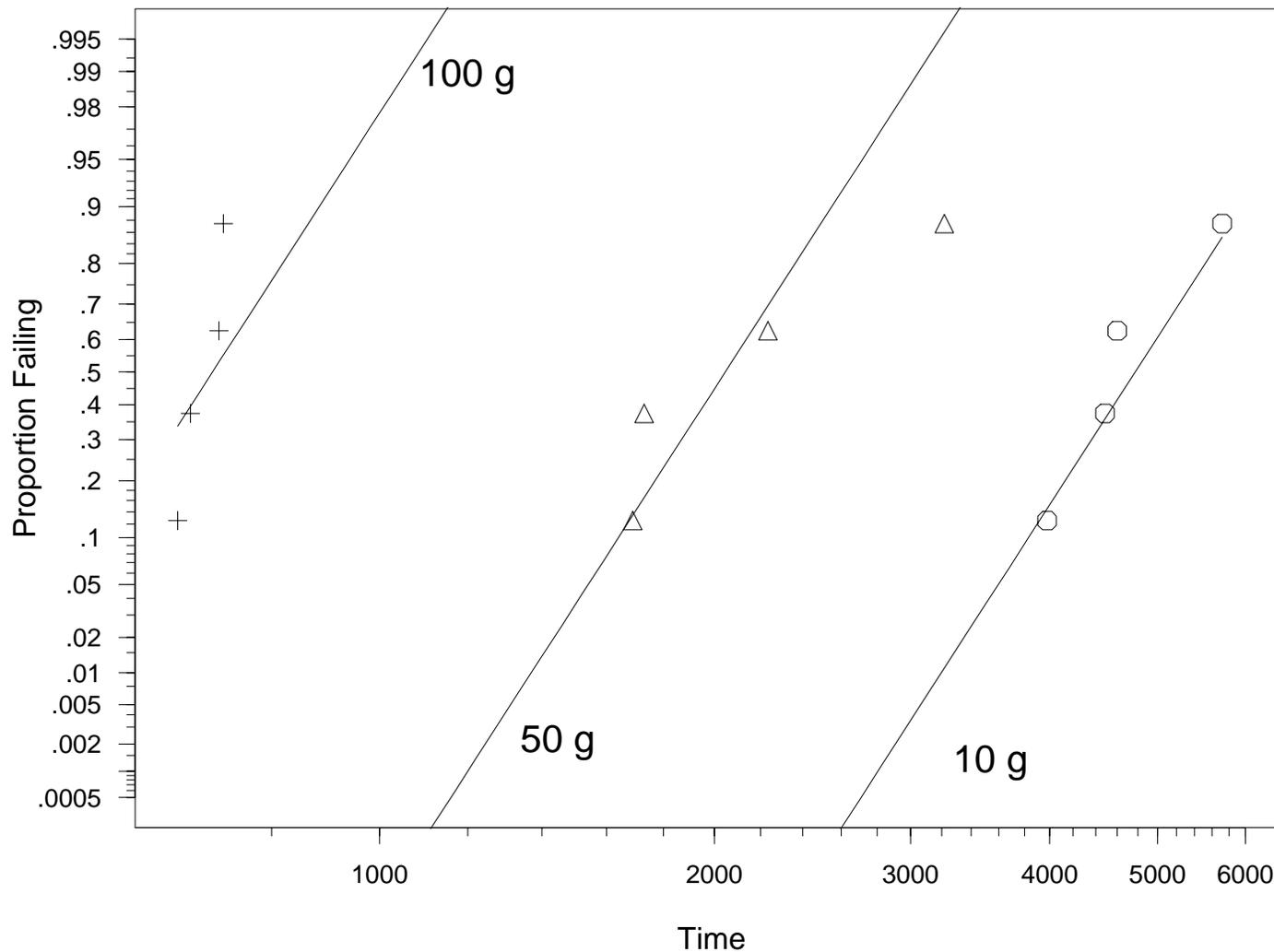
# Pseudo Failure Time to 50 Microns Scar Width Versus Applied Weight for the Metal-to-Metal Sliding Test



# Lognormal Probability Plot Showing the ML Estimates of Time to 50 Microns Width for Each Weight



# Lognormal Probability Plot Showing the Lognormal Regression Model ML Estimates of Time to 50 Microns Width for Each Weight



## Other Topics in Chapter 21

- Choice of parameter transformation in the estimation/bootstrap procedure.
- Stochastic process degradation models.

Test planning case study in Chapter 22.